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Parameter optimization with respect to elongated hillock regions beside the high-speed railway under crosswinds

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Abstract

Complex terrains will result in elongated hillocks occurring near the windbreak wall along high-speed railways, furthermore, the hillock weakens the anti-wind ability of the windbreak wall. In this paper, characteristic parameters - the distance between hillock and windbreak wall (*D*) and the hillock height (*H*) are optimized by capitalizing on computational fluid dynamics (CFD) and multi-objective optimization method of the Non-dominated Sorting Genetic Algorithm II (NSGA-II). The surrogate model of Kriging model is advantaged and it is to be the final surrogate model to optimize the maximum wind speed U_{max} and peak-to-peak value $U_{p\cdot p}$ for the railway concerned. The optimized results demonstrate that D = 25 - 35 m and H = 2 - 12 m can ensure that $U_{\text{max}} < 0.5$. Besides, it is shown that distance *D* plays a key role in reducing the sudden wind peak values.

Keywords: windbreak wall, crosswind, high-speed railway, NSGA-II.

1 Introduction

The effect of strong winds on trains is an intractable problem all over the world and attracts many researchers' attention [1, 2]. In China, part of the railway passes through the strong wind area, and diverse windproof facilities are constructed to mitigate the

wind impact [3], including the vertical plate-type windbreak wall, open-hole antiwind tunnel, and porous windbreak wall, etc. Owing to complicated terrains along the railway, different transition regions generated beside the railway and impair the antiwind property of windproof facilities. The effect of these transition regions has been studied in detail by Sun et al.[4]

Generally, Unified and continuous windbreak walls with a height of 3.5 m or 4 m provide the capability of ensuring the safe operation for the high-speed train. However, the full-scale test found that the train had a remarkable yawing phenomenon in some regions with uniform 3.5 m high windbreak wall. After conducting on-site investigations and comparing the time-history aerodynamic forces combined with the railway mileages, it indicated that some elongated hillocks near the windbreak occurred. The height of such hillocks is equivalent to or higher than the height of the windbreak wall. Thereby, the windproof ability of the windbreak wall is weakened greatly [5].

To account for the effect of elongated hillocks, this paper optimizes the flow structures and obtains a rational range of the height (*H*) of hillock and the distance (*D*) from the windbreak wall. The optimization targets are the maximum value and peak-to-peak value of the wind speed coefficient (U_{max} and U_{p-p}) in the center of railway. The wind speed coefficient is defined as the ratio between the wind speed in the railway and the wind speed outside the windbreak wall. As shown in Figure 1, by considering real conditions, the optimal range of *D* is 0 - 60 m and the optimal range of *H* is 2 - 12 m.

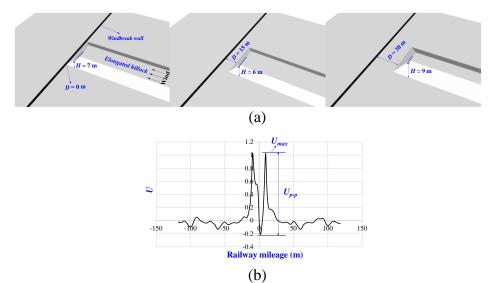


Figure 1: The optimization parameters and targets: (a) the distance D and hillock height H, (b) the optimization targets U_{max} and U_{p-p} .

2 Methods

The optimization method utilized in this paper is the Non-dominated Sorting Genetic Algorithm II (NSGA-II), and the sample points are picked out by the optimal Latin

hypercube (OLH) design method. The total 13 samples are calculated by the computational fluid dynamics (CFD) method.

Based on the commercial CFD code Fluent, the improved delayed detached eddy simulation (IDDES) method with SST $k-\omega$ turbulence model is chosen to analyse the wind field and the distribution of U_{max} and U_{p-p} . The traditional detached eddy simulation (DES) method potentially produces modeled-stress depletion (MSD), which in some situations can lead to early separation, namely the grid-induced separation (GIS) effect. This effect is related to the grid spacing rather than to the physical properties of turbulence. The IDDES is a hybrid method combining the delayed detached eddy simulation (DDES) and wall-modeled large eddy simulation (WMLES), offers advantages for overcoming MSD and GIS, and for reducing the limitation of the Reynolds number for near-wall flow. The IDDES method has achieved enormous success in the field of train aerodynamics and flow analysis [6]. In addition, the surrogate model should be established to carry out the optimization process by NSGA-II. The algorithm of NSGA-II can reduce the computational complexity while ensuring the diversity of the population, and it is accompanied by a high optimization efficiency [7]. Disparate surrogate models are compared in this work, such as the response surface model (RSM), radial basis function neural network (RBFNN), and Kriging model. The detailed optimization process can refer to Chen and Ni [8].

3 Results

The coefficient of determination, R^2 , of different surrogate models is tabulated in Table 1. R^2 of the Kriging model for U_{max} and U_{p-p} is 0.895 and 0.936, respectively. Therefore, the Kriging model is chosen as the surrogate model to implement the optimization process by the NSGA-II method. Furthermore, the relationship between design variables and optimization goals are demonstrated in Figure 2. Comparing the effect of parameter variables D and H, it can be found that the influence of D is greater.

The relationship between U_{max} and U_{p-p} is depicted in Figure 3(a), due to backflows are not strong, the U_{p-p} is larger than U_{max} slightly. As shown in Figure 3(b), in the situation where $U_{max} < 0.5$, the corresponding D and H are 25 – 35 m and 2 – 12 m, respectively. Also, as long as the hillock is far enough from the windbreak wall, the effect of hillock height can be negligible. To verify the reliability of optimized and predicting results, extra three cases are computed by CFD. As illustrated in Figure 4 and Table 2, the error (defined in Equation (1)) for U_{max} is less than 8%, and the discrepancy for U_{p-p} is less than 5%. The deviation of U_{max} is larger on account of the small base value. Overall, the optimized and prediction results are in good agreement with the CFD results, which can be taken as a reference to guide actual construction.

Target parameters	RSM	RBFNN	Kriging
U_{max}	0.758	0.857	0.895
U_{p-p}	0.565	0.643	0.936

Table 1: The coefficient of determination, R^2 , of different surrogate models.

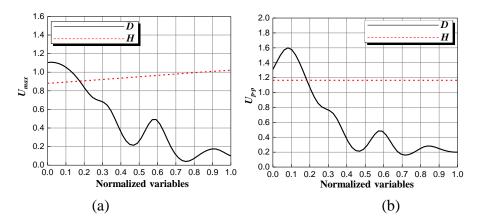


Figure 2: The relationship between the optimization parameters and targets: (a) U_{max} , (b) U_{p-p} .

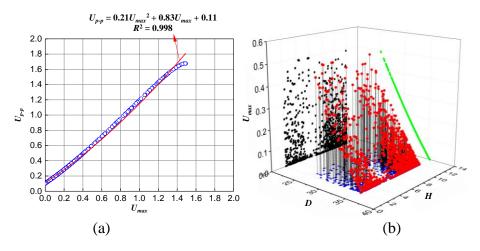


Figure 3: (a) The relationship between U_{max} and U_{p-p} , (b) the range of D and H when $U_{max} < 0.5$.

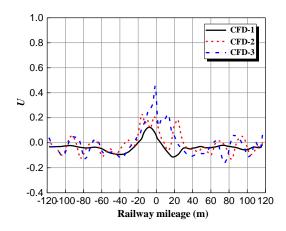


Figure 4: Three test cases of CFD results.

$$Error = \left| \frac{U_{prediction} - U_{CFD}}{U_{CFD}} \right| \tag{1}$$

No.	<i>D</i> (m)	<i>H</i> (m)	Umax			U_{p-p}		
			Prediction	CFD	Error	Prediction	CFD	Error
1	32.81	3.88	0.105	0.112	6.25%	0.196	0.205	4.39%
2	29.78	9.71	0.237	0.221	7.24%	0.332	0.317	4.73%
3	24.67	5.67	0.513	0.486	5.56%	0.618	0.598	3.34%

Table 2: Comparison between the prediction and CFD results.

4 Conclusions and Contributions

Employing the computational fluid dynamics (CFD) and the Non-dominated Sorting Genetic Algorithm II (NSGA-II), this study figured out the parameter optimization of a characteristic elongated hillock region beside a railway.

By adopting the optimal Latin hypercube design, 13 sample points are obtained to conduct the CFD simulation. Among three surrogate models, the Kriging model shows a good representation ability on the wind speed coefficient of U_{max} and U_{p-p} in the railway.

The research results indicate that the distance (D) from the hillock to the windbreak wall is a critical variable, and the hillock height *H* is a minor factor. In cases studied in this paper, to meet the peak value of wind speed coefficient $U_{max} < 0.5$, the corresponding optimized parameters D = 25 - 35 m and H = 2 - 12 m are recommended

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